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BOOK OF PAPERS

1992 International Conference & Exhibition

Optimum Conditions for Sequential Oxidative/Reductive Bleaching of Wool in a Single Bath

Jeanette M. Cardamone, William N. Marrner and Mustafa Arifoglu
 USDA, ARS, Eastern Regional Research Center, Philadelphia, Pa., and
 Herbert J. Barndt, Philadelphia College of Textiles and Science, Philadelphia

ABSTRACT

Conventional bleaching of wool with alkaline H₂O₂ was compared to variations of the ARS single-bath sequential oxidation/reduction bleaching process. The ARS process involves peroxide bleaching (Step 1), then *in-situ* formation of thiourea dioxide from the reaction of thiourea with unspent peroxide (Step 2). Subsequent hydrolysis of thiourea dioxide forms the reducing agent, sulfinate ion, with urea as by-product, and reductive bleaching ensues.

Mechanistic studies for this reaction, using ¹³C solution NMR in the absence of wool, showed the appearance of urea as a marker for the conversion of thiourea dioxide to sulfinate. In all but the mildest bleaching conditions, the conversion of thiourea dioxide was immediate and complete. Only under the mildest conditions (50°C, 8 g/L peroxide, pH 7.8 for the reductive bleaching step) did a stable thiourea dioxide signal appear, and this disappeared upon the addition of wool.

In bleaching studies on wool challis, we compared conventional peroxide bleaching using 22 g/L (20 mL/L) 30% hydrogen peroxide at 50°C and 60°C with various ARS single-bath compositions: (a) 16 g/L; or (b) 8 g/L in Step 1 followed by the addition of thiourea (70% of the weight of peroxide) in Step 2; or (c) 22 g/L peroxide in Step 1 followed by modifying the bath to reach an effective peroxide level of 16 g/L and 8 g/L before the addition of thiourea.

Results indicated that various levels of whiteness can be achieved that equal or surpass conventional alkaline bleaching carried out within the same time and temperature limits. Physical testing of the ARS-bleached fabrics showed them to have achieved comparable or improved whiteness (up to 8 WI units) over the conventionally bleached fabrics. By Instron testing, the whiter ARS-bleached samples have no more than an 11% loss in specific stress, with only slight changes in elastic moduli and % strain at peak stress.

These fabrics were also analyzed by the KES system. The ARS-bleached challis showed measurable decreases in shear stiffness and in bending and shear hystereses, as well as increases in maximum extension. These factors contribute to the overall fabric-handle expression "Shinayakasa," the values of which indicated greater softness, flexibility and smooth feeling for the ARS-bleached fabrics.

INTRODUCTION

The processing of wool most often includes its bleaching to remove stain and, occasionally, black hair contamination. The most effective bleaching regimens for stain incorporate both an oxidative and a reductive bleaching step and are referred to as "full" bleaching. Such full bleaching is normally a two- or three-step process carried out in separate baths. Initial oxidative bleaching normally makes use of hydrogen peroxide. Subsequent reductive bleaching uses such agents as dithionite, sodium formaldehyde sulfoxylate or thiourea dioxide (1).

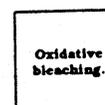
In a series of recent reports (2-6), patents and patent applications (7-12), we have reported on the development of new approaches to full bleaching that integrate the processes into single-bath procedures (Figure 1).

Bleaching for Stain Only

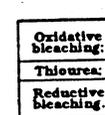
MOST COMMONLY PRACTICED:



MOST EFFECTIVE METHOD IN PRACTICE:



NEW ERRC PROCESS:



Bleached Product

(Figure 1)

By conventional processes, initial bleaching with hydrogen peroxide is interrupted by quenching. Residual peroxide can simply be destroyed catalytically and a subsequent reductive bleaching carried out by addition of reducing bleach. In the ERRC ARS process, residual peroxide is best utilized in a quick chemical reaction that converts the bath into a reductive medium. When thiourea is added under controlled conditions to the peroxide bath, thiourea dioxide is produced. It then hydrolyzes to sulfinate — the reductive bleaching species (2, 4-8, 11, 12).

Bleaching for black-hair removal typically is done by initial mordanting with ferrous sulfate, then controlled rinsing to eliminate all iron except that which is selectively adsorbed onto the black fibers. Then, hydrogen peroxide is added, black hairs are bleached by a radical mechanism induced by adsorbed iron, and overall stain is bleached concomitantly (14). Here again, we have found that residual peroxide may be utilized by conversion of the bleach bath to a reducing medium by controlled addition of thiourea (Figure 2).

Bleaching for Black Hair and Stain

MOST COMMONLY PRACTICED:



MOST EFFECTIVE METHOD IN PRACTICE:



NEW ERRC PROCESS:



Bleached Product

TABLE I. Conditions for ARS Bleaching, Optimization Runs

SAMPLE NAME	Step 1		Step 2		T (°C)
	[H ₂ O ₂] (g/L)	t (min)	[H ₂ O ₂] (g/L)	t (min)	
STD6000	0	85	(no Step 2)		60
STD5000	0	85	(no Step 2)		50
CON6022	22	85	(no Step 2)		60
CON5022	22	85	(no Step 2)		50
ARS6016	16	60	16	25	60
ARS5016	16	60	16	25	50
ARS6008	8	60	8	25	60
ARS5008	8	60	8	25	50
ARS5512	12	60	12	25	55
MOD6016	22	60	16	25	60
MOD5016	22	60	16	25	50
MOD6008	22	60	8	25	60
MOD5008	22	60	8	25	50

Measurements of Fabric Properties

Whiteness Index (WI; ASTM E-313; 3.3872 - 3Y) and Yellowness Index (YI; ASTM D-1925; 100 [1.277X - 1.06Z]/Y) were measured on The Color Machine spectrophotometer (BYK Gardner). Measurements were made using 360° circumferential illumination by a quartz halogen lamp at a color temperature of 2854 K (CIE Source C illuminant, CIE Standard 2° observer) at a 45° angle from the sample's normal direction, with sample viewing at 0°.

Fabric Handle

The Kawabata Evaluation System (KES) was used to examine the fabric's physical and mechanical properties, using weight, thickness, and tensile bending, shearing, and compression data.

Instron Testing

Fabrics were measured for specific stress, elastic moduli, and percentage strain at peak stress on an Instron Model 1122 analyzer. Analyses were carried out according to ASTM 1682-64, Raveled Strip method for wet specimens (Section 17.2) with 23 kg (50 pound) load cell (Instron 2511-103) and full range switch setting 50 for 50-pound full-scale load deflection. Crosshead speed was 200 mm/sec to allow the fabric strip to break within 23 sec during the test. Force to break was normalized to the fabric linear density (g/cm) with specific stress reported as N*cm/g.

NMR Spectroscopy

All ¹³C-NMR spectra were obtained on a Bruker MSL-300 instrument operating at 75.5 MHz. All spectra were obtained with a 9 microsec (80°) pulse with a recycle time of 10 sec. Each spectrum was obtained from 66 8K-data-point scans. Temperature was controlled to within ± 1°C.

We examined the 8 and 16 g/L (Step 2) reactions at 50°C and 60°C and at pH ranges of 7.1-7.8 and 8.4-8.9. The procedure involved preparing 15 mL stock solutions of 8 g/L (1.07 x 10⁻³ mol) peroxide and 16 g/L (2.14 x 10⁻³ mol) peroxide. The corresponding amounts of thiourea required were 3.3 x 10⁻⁴ mol and 6.6 x 10⁻⁴ mol, respectively, wherein the peroxide to thiourea molar ratio was 3:2 in each case. Aliquots (3 mL) were taken for each NMR analysis.

RESULTS

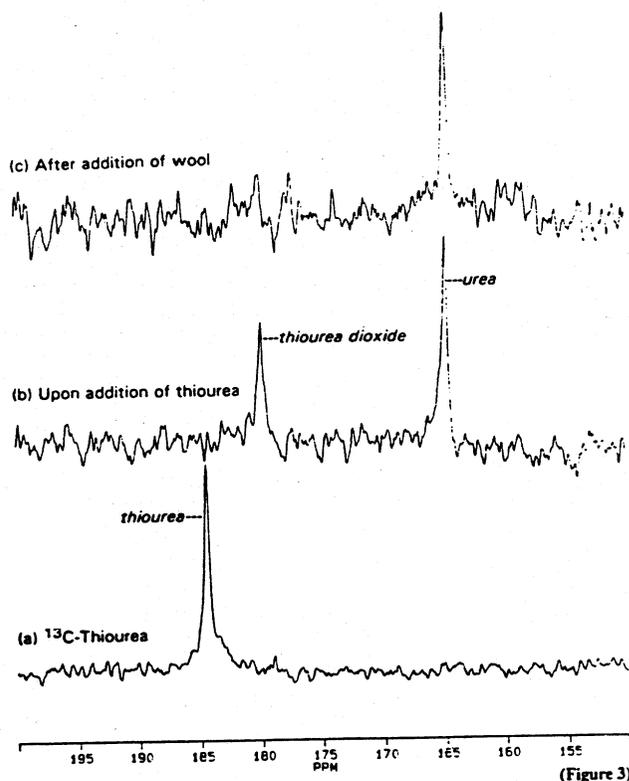
Reaction Mechanism

The NMR spectrum of ¹³C-thiourea (Figure 3a) was not stable in the presence of hydrogen peroxide at pH 4.5-5.5, but changed instead to the signal for thiourea dioxide (179.8 ppm). When the pH then was raised to >7, complete reaction of the thiourea dioxide was seen, leaving only a signal for the reaction product urea (164.7 ppm). Under the mildest bleaching conditions

(8 g/L, 50°C, pH 7.8), however, the thiourea dioxide signal remained pronounced along with the new signal for urea (Figure 3b). Complete conversion to urea in that case was observed (Figure 3c) only after wool was added and stirred into the bleaching solution.

¹³C NMR STUDY OF ARS BLEACHING PROCESS

[H₂O₂] = 8 g/L; 50°C; final pH 7.8



These findings support the work of others who found that the decomposition of thiourea dioxide is controlled by the effect of temperature and time with higher temperature causing greater decrease in thiourea dioxide in the absence of wool. In the presence of wool there was an obvious acceleration of the rate of decomposition of thiourea dioxide (15).

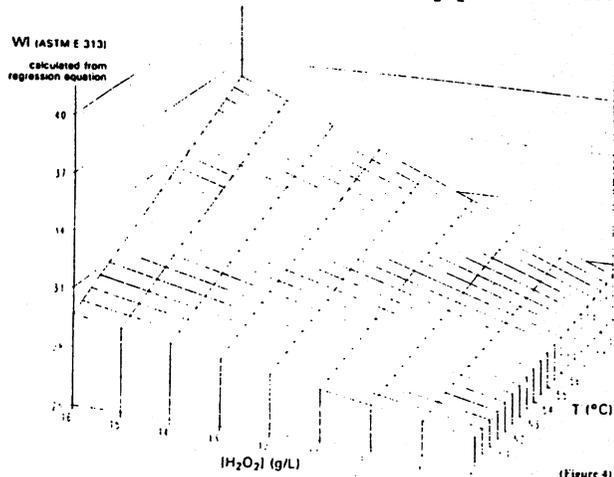
Whiteness and Yellowness

The average values for whiteness index WI and yellowness index YI for 18 replications for each bleaching condition are reported as observed values and have been analyzed for statistical differences. The estimated values used to formulate the graphs in Figures 4 and 5 were derived from the method of least squares from the multiple regression equations 4 and 5 to describe the influence of temperature (T), peroxide concentration [H₂O₂], and the combined effects:

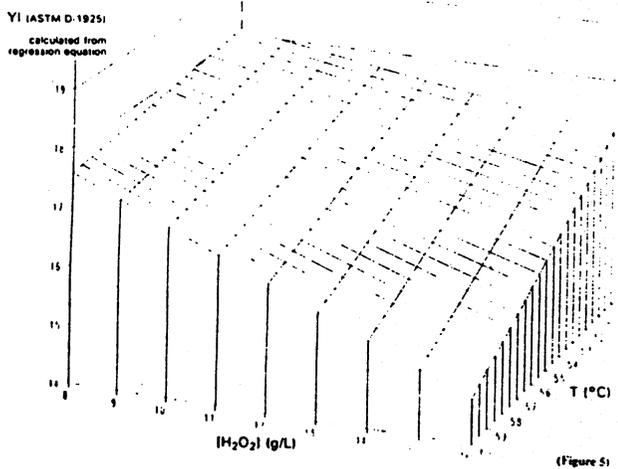
$$WI = 43.745 - 0.42T - 2.89 [H_2O_2] + 0.066T [H_2O_2] \quad \text{EQ. 4} \\ (R^2=0.918)$$

$$YI = 13.04 + 0.123T + 0.973 [H_2O_2] - 0.022 T [H_2O_2] \quad \text{EQ. 5} \\ (R^2=0.900)$$

EFFECT OF TEMPERATURE AND [H₂O₂] ON WHITENESS

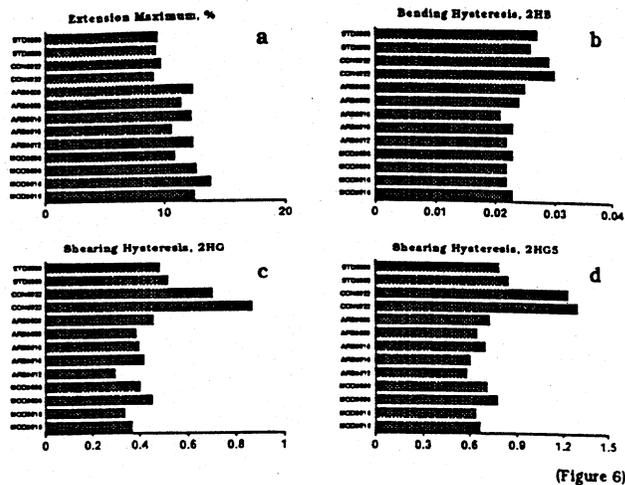


EFFECT OF TEMPERATURE AND [H₂O₂] ON YELLOWNESS

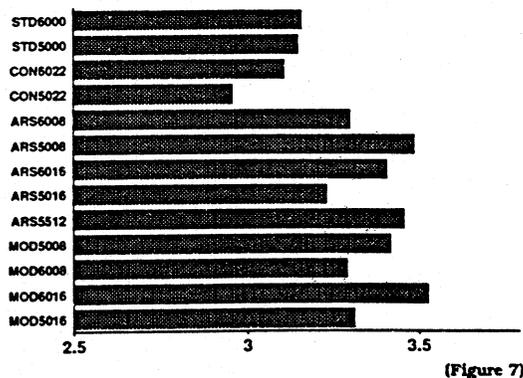


Fabric Handle

Evaluation of fabric handle by the Kawabata Evaluation System (KES-F) was made on three fabrics selected randomly from the 18 replications per bleaching condition. Each fabric was tested three times in the warp and three times in the weft directions for a total of 6 evaluations. The most pronounced differences (Figure 6, a-d) when conventional and ARS fabrics are compared are in the parameters EM₁ (extension maximum at 500 g/cm) in (a), 2HB (Bending Hysteresis) in (b), 2HG (Shearing Hysteresis at 0.5° shear angle) in (c), and in 2HG5 (Shearing Hysteresis at 5° shear angle) in (d). The hand expression suitable for thin fabrics, in particular for women's thin dress fabric is the Kawabata term, "Shinayakasa" (16), which indicates softness, flexibility, and smooth feeling. Shinayakasa results are shown in Figure 7.

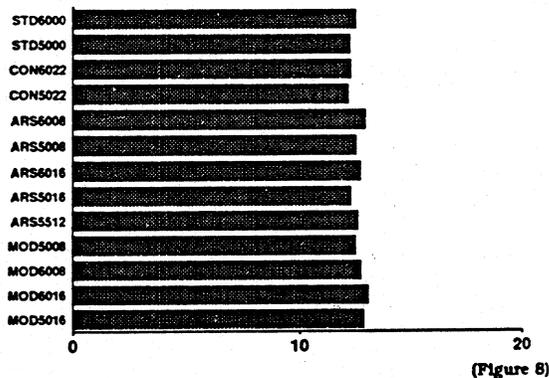


Shinayakasa



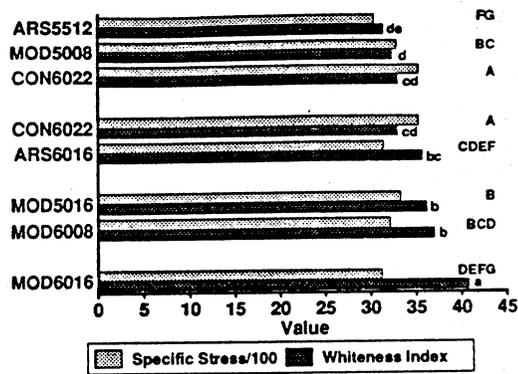
The KES system also provides the "W" parameter for weight per unit area in mg/cm² in Figure 8. It can be used in reference to chemical damage for comparing the after-effects of wool bleaching.

Weight per unit area, W

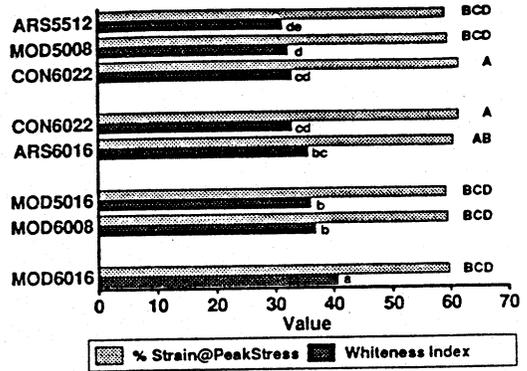
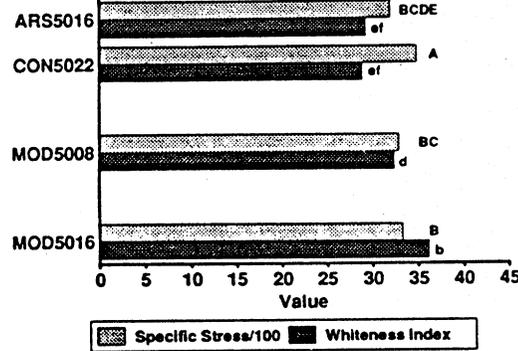


Mechanical Property Testing

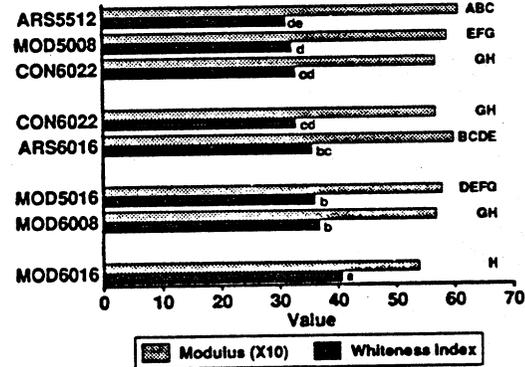
Results from Instron testing are given in Figures 9-11. Solid bars indicate whiteness (WI) and shaded bars indicate the mechanical property (specific stress, elastic modulus, and percent strain at peak stress, respectively). In each figure, the top set compares all bleachings (50 and 60°C) shown to give equivalent or better whiteness than the conventionally bleached sample CON6022. The bottom set compares all 50°C bleachings that gave equivalent or better whiteness than CON5022 (itself a 50° bleaching). All bars labelled with a common letter are not statistically different (p<.005).



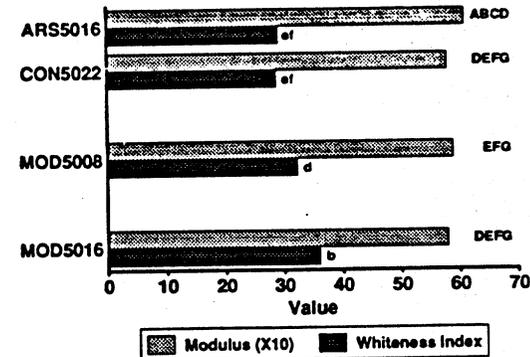
(Figure 9)



(Figure 11)



(Figure 10)



DISCUSSION

Relative to conventional bleaching at 60°C (CON6022; 85 min oxidative bleaching only; [H₂O₂] = 22 g/L, WI = 33), the following observations were made: (Note that **bold entries** are statistically different; *italicized* are not [p<.005].)

To achieve the same degree of whiteness, use the conditions of ARS5512 (drop T to 55°C; use only 12 g/L H₂O₂ (WI = 31)). This results in the following mechanical and KES properties:

- 14% loss in specific stress.
- 7% increase in elastic modulus.
- 4% reduction in % strain at peak stress.
- KES Shinayakasa: 111%
- KES Bending Hysteresis 2HB: 75%
- KES Shear Stiffness G: 80%
- KES Shearing Hysteresis (0.5 deg) 2HG: 43%
- KES Shearing Hysteresis (5.0 deg) 2HG5: 48%
- KES Maximum Extension @500 g/cm, EM%: 128%

or use the conditions of MOD5008 (drop T to 50°C; start at 22 g/L H₂O₂, but reduce to 8 g/L (WI = 32):

- 7% loss in specific stress.
- No change in elastic modulus.
- 3% reduction in % strain at peak stress.
- KES Shinayakasa: 110%
- KES Bending Hysteresis 2HB: 78%
- KES Shear Stiffness G: 88%
- KES Shearing Hysteresis (0.5 deg) 2HG: 58%
- KES Shearing Hysteresis (5.0 deg) 2HG5: 58%
- KES Maximum Extension @500 g/cm, EM%: 112%

or use the conditions of ARS6016 (keep T at 60°C; use only 16 g/L H₂O₂ (WI = 36):

- 11% loss in specific stress.
- 5% increase in elastic modulus.
- No change in % strain at peak stress.
- KES Shinayakasa: 110%
- KES Bending Hysteresis 2HB: 73%
- KES Shear Stiffness G: 85%
- KES Shearing Hysteresis (0.5 deg) 2HG: 57%
- KES Shearing Hysteresis (5.0 deg) 2HG5: 57%
- KES Maximum Extension @500 g/cm, EM%: 126%

To achieve better whiteness using an ARS process, use the conditions of MOD5016 (drop T to 50°C; start at 22 g/L H₂O₂, but reduce to 16 g/L for Step 2 (WI = 36):

- 6% loss in specific stress.
- No change in elastic modulus.
- 4% reduction in % strain at peak stress.
- KES Shinayakasa: 106%
- KES Bending Hysteresis 2HB: 78%
- KES Shear Stiffness G: 86%
- KES Shearing Hysteresis (0.5 deg) 2HG: 53%
- KES Shearing Hysteresis (5.0 deg) 2HG5: 54%
- KES Maximum Extension @500 g/cm, EM%: 129%

or use the conditions of MOD6008 (keep T at 60°C; start at 22 g/L H₂O₂, but reduce to 8 g/L for Step 2 (WI = 37):

- 9% loss in specific stress.
- No change in elastic modulus.
- 3% reduction in % strain at peak stress.
- KES Shinayakasa: 106%
- KES Bending Hysteresis 2HB: 75%
- KES Shear Stiffness G: 87%
- KES Shearing Hysteresis (0.5 deg) 2HG: 65%
- KES Shearing Hysteresis (5.0 deg) 2HG5: 63%
- KES Maximum Extension @500 g/cm, EM%: 130%

To achieve the best whiteness using an ARS process, use the conditions of MOD6016 (keep T at 60°C; start at 22 g/L H₂O₂, but reduce to 16 g/L for Step 2 (WI = 41):

- 11% loss in specific stress.
- No change in elastic modulus.
- 3% reduction in % strain at peak stress.
- KES Shinayakasa: 114%
- KES Bending Hysteresis 2HB: 77%
- KES Shear Stiffness G: 83%
- KES Shearing Hysteresis (0.5 deg) 2HG: 48%
- KES Shearing Hysteresis (5.0 deg) 2HG5: 52%
- KES Maximum Extension @500 g/cm, EM%: 142%

We may also compare the conventional bleaching run at 50°C (CON5022, 85 min oxidative bleaching only, (WI = 29)) to the ARS bleaching runs done at 50°C:

To achieve the same degree of whiteness, use the conditions of ARS50 16 (16 mL/L H₂O₂ (WI = 29):

- 8% loss in specific stress.
- No change in elastic modulus.
- 3% increase in % strain at peak stress.
- KES Shinayakasa: 109% of CON5022
- KES Bending Hysteresis 2HB: 76%
- KES Shear Stiffness G: 85%
- KES Shearing Hysteresis (0.5 deg) 2HG: 48%
- KES Shearing Hysteresis (5.0 deg) 2HG5: 47%
- KES Maximum Extension @500 g/cm, EM%: 116%

For better whiteness, use the conditions of MOD5008 (start at 22 mL/L H₂O₂, but reduce to 8 mL/L for Step 2 (WI = 32):

- 6% loss in specific stress.
- No change in elastic modulus.
- 2% increase in % strain at peak stress.
- KES Shinayakasa: 116% of CON5022
- KES Bending Hysteresis 2HB: 76%
- KES Shear Stiffness G: 88%
- KES Shearing Hysteresis (0.5 deg) 2HG: 47%
- KES Shearing Hysteresis (5.0 deg) 2HG5: 55%
- KES Maximum Extension @500 g/cm, EM%: 120%

For the best whiteness at 50°C, use the conditions of MOD5016 (start at 22 g/L H₂O₂, but reduce to 16 g/L for Step 2 (WI = 36):

- 4% loss in specific stress.
- No change in elastic modulus.
- No change in % strain at peak stress.
- KES Shinayakasa: 112% of CON5022
- KES Bending Hysteresis 2HB: 76%
- KES Shear Stiffness G: 85%
- KES Shearing Hysteresis (0.5 deg) 2HG: 43%
- KES Shearing Hysteresis (5.0 deg) 2HG5: 51%
- KES Maximum Extension @500 g/cm, EM%: 137%

CONCLUSION

The most pronounced property changes were in whiteness, strength, and fabric handle. We have shown that the whiteness indices (WI) for ARS-bleached fabrics using less peroxide compare to or surpass the WI for fabrics bleached by the conventional process.

All ARS-bleached samples were up to 11% weaker than conventionally bleached fabrics CON6022 and CON5022 at 60° and 50°C. Statistically, there were no differences in specific stress among all ARS-bleached fabrics at 50°C, but all were weaker yet whiter than the conventionally bleached CON5022. Statistically, ARS fabrics bleached at the higher temperature, 60°C, were except for MOD6008 weaker than fabrics bleached at 50°C, and they were weaker than conventionally bleached CON6022.

Regarding determinations of elastic modulus, run on the Instron analyzer, only two of the ARS bleachings showed significant changes (slight increases, ≤7%) from the conventional bleachings. Regarding percent strain at peak stress, also run on the Instron analyzer, most ARS samples broke at a slightly lower extension (≤5%) than the conventional runs.

The KES studies provide a better examination of mechanical properties under slight deformation, which correlate better to fabric handle than the Instron-derived values. Figures for maximum extension @500 g/cm indicate markedly higher extensions (up to 142%) for the ARS samples. These differences and those seen for shearing and bending properties all contribute to the KES expression "Shinayakasa," for improved softness, flexibility and smooth feeling. The ARS samples fell in a range of 109 to 116% of the CON6022 value.

Although there is a slight trade-off in strength loss of 6 to 11%, the advantage to using ARS bleaching is better whiteness, softer handle and a savings in energy. Energy is conserved, of course, when the process is run at 50°C. However, if we compare the ARS single-bath process to "full" conventional bleaching (oxidative in one bath and reductive in another), further energy savings are obvious. An added bonus is that the spent ARS bath contains sulfate from oxidized sulfinate and urea from reacted thiourea dioxide; these products are dye-assists for subsequent dyeing when the ARS-bleaching technology is expanded to include dyeing in the same bath (5).

Although chemical analysis for protein damage to wool has not been completed for the latest study, earlier studies of alkali solubility indicated no deterioration (2). Furthermore, the KES fabric weight determinations (W) for all samples presented here appear to be the same (Figure 8), supportive of minimal damage by alkali.

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